A Convex Approach to Hydrodynamic Analysis

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Abstract—We study stability and input-state analysis of three dimensional (3D) incompressible, viscous flows with invariance in one direction. By taking advantage of this invariance property, we propose a class of Lyapunov and storage functionals. We then consider exponential stability, induced \mathcal{L}^2 -norms, and input-to-state stability (ISS). For streamwise constant flows, we formulate conditions based on matrix inequalities. We show that in the case of polynomial laminar flow profiles the matrix inequalities can be checked via convex optimization. The proposed method is illustrated by an example of rotating Couette flow.

I. INTRODUCTION

The dynamics of incompressible fluid flows is described by a set of nonlinear partial differential equations known as the Navier-Stokes equations. The properties of such flows are then characerized in terms of a dimensionless parameter Re called the Reynolds number. Experiments show that many flows have a critical Reynolds number Re_C below which global stability is ensured. However, spectrum analysis of the linearized Navier-Stokes equations, considering only infinitesimal perturbations, predicts a linear stability limit Re_L which upper-bounds Re_C [1]. On the other hand, the bounds using energy methods Re_E , the limiting value for which the energy of arbitrary large perturbations decreases monotonically, are much below Re_C [2]. For example, $Re_E = 32.6$ [3], $Re_L = \infty$ [4] and $Re_C = 350$ [5] for 3D Couette flow.

The discrepancy between Re_L and Re_C have long been attributed to the eigenvalues analysis approach [6], citing a phenomenon called $transient\ growth$; i.e., although the perturbations to the linearized Navier-Stokes equation are stable, they undergo high amplitude transient amplifications that steer the trajectories out of the region of linearization. This has led to studying the resolvent operator or ε -pseudospectra based on the general solution to the linearized Navier-Stokes equations [7]. Another method for studying stability is based on spectral truncation of the Navier-Stokes equations into an ODE system. Recently in [8], [9], a method was proposed based on keeping a number of modes from Galerkin expansion and bounding the energy of the remaining modes. However, these bounds on Re_C turn out to be conservative.

Since the seminal paper by Reynolds [10], it was observed that external excitations and body forces play an important

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role in flow instabilities. Mechanisms such as energy amplification of external excitations have shown to be crucial in understanding transition to turbulence [2]. Energy amplification of stochastic forcings to the linearized Navier-Stokes equations in parallel channel flows was studied in [11], [12]. In [12], using the linearized Navier-Stokes equation, it was shown analytically, through the calculation of traces of operator Lyapunov equations, that the \mathcal{H}^2 -norm from streamwise constant excitations to perturbation velocities is proportional to Re^3 . The $O(Re^3)$ amplification mechanism of the linearized Navier-Stokes equation was verified in [13] and [14], where the influence of each component of the body forces was calculated in terms of \mathcal{H}^2 and \mathcal{H}^{∞} -norms. Inputoutput analysis of a model of plane Couette flow was carried out in [15] to study the nonlinear mechanisms associated with turbulence. In another vein, an input-state analysis method for the linearized Navier-Stokes equation by calculating the spatio-temporal impulse responses was given in [16].

In this paper, we study the stability and input-state properties of incompressible, viscous fluid flows. We study input-state properties such as induced \mathcal{L}^2 -norms from body forces to perturbation velocities and ISS. In particular, we consider flows with invariance in one of the three spatial coordinates. For such flows, we formulate a suitable structure as a Lyapunov/storage functional. Then, based on these functionals, for streamwise constant flows, we propose conditions based on matrix inequalities. In the case of polynomial laminar velocity profiles, e.g. Couette and Poiseuille flows, these inequalities can be checked via convex optimization using available computational tools. The proposed method is applied to the analysis problem of a rotating Couette flow.

The paper is organized as follows. The next section presents some preliminary results. In Section III, we formulate the Lyapunov/storage functional structure. Section IV is concerned with the convex formulation for streamwise constant flows. The proposed method is illustrated by studying an example of a model of rotating Couette flow in Section V. Finally, Section VI concludes the paper and provides directions for future research.

Notation: The n-dimensional Euclidean space is denoted by \mathbb{R}^n . The $n\times n$ identity matrix is denoted by $\mathrm{I}_{n\times n}$. A domain $\Omega\subset\mathbb{R}^n$ is a connected, open subset of \mathbb{R}^n , and $\overline{\Omega}$ is the closure of set Ω . The boundary $\partial\Omega$ of set Ω is defined as $\overline{\Omega}\setminus\Omega$ with \setminus denoting set subtraction. The space of p-th power integrable functions defined over Ω is denoted \mathcal{L}^p_Ω endowed with the norm $\|(\cdot)\|_{\mathcal{L}^p_\Omega}=\left(\iint_\Omega(\cdot)^p\ \mathrm{d}\Omega\right)^{\frac{1}{p}}$, for $1\leq p<\infty$, and $\|(\cdot)\|_{\mathcal{L}^\infty_\Omega}=\sup_{x\in\Omega}|(\cdot)|$, for $p=\infty$. Also, we denote

by $\mathcal{L}^2_{[t_0,T],\Omega}$, with $t_0 \geq 0$, the space of square integrable functions in $x \in \Omega$ and $t \in [t_0,T]$ with the norm

$$\|(\cdot)\|_{\mathcal{L}^2_{[t_0,T),\Omega}} = \left(\int_{t_0}^T \|u\|_{\mathcal{L}^2_{\Omega}}^2 dt\right)^{\frac{1}{2}}.$$

The space of k-times continuous differentiable functions defined on Ω is denoted by $\mathcal{C}^k(\Omega)$. If $p \in \mathcal{C}^1$, then $\partial_{x_1} p$ is used to denote the derivative of p with respect to variable x_1 , i.e. $\partial_{x_1} := \frac{\partial}{\partial x_1}$. A continuous strictly increasing function $k:[0,a)^p \to \mathbb{R}_{\geq 0}$, satisfying k(0)=0, belongs to class \mathcal{K} . If $a=\infty$ and $\lim_{x\to\infty} k(x)=\infty$, k belongs to class \mathcal{K}_∞ . The unit vector in direction x_i is denoted by \overrightarrow{e}_i . For a scalar function $v,\nabla v=\sum_i\partial_{x_i}v\overrightarrow{e}_i$ denotes the gradient and $\nabla^2 v=\sum_i\partial_i^2 v$ denotes the Laplacian. For a vector valued function $\mathbf{w}=\sum_i w_i \overrightarrow{e}_i$, the divergence $\nabla \cdot \mathbf{w}$ is given by $\nabla \cdot \mathbf{w}=\sum_i\partial_{x_i}w_i$.

II. PRELIMINIARIES

A. Flow Model

We consider incompressible, viscous flows with invariance in one of the directions x_m , $m \in \{1, 2, 3\}$, i.e., $\partial_{x_m} = 0$. Let $I = \{1, 2, 3\} - \{m\}$. The flow dynamics is described by the Navier-Stokes equations, given by

$$\partial_{t}\bar{\boldsymbol{u}} = \frac{1}{Re}\nabla^{2}\bar{\boldsymbol{u}} - \bar{\boldsymbol{u}}\cdot\nabla\bar{\boldsymbol{u}} - \nabla\bar{p} + F\bar{\boldsymbol{u}} + \boldsymbol{d},$$

$$0 = \nabla\cdot\bar{\boldsymbol{u}}, \tag{1}$$

where t>0, $F\in\mathbb{R}^{3\times3}$, and $\mathbf{x}\in\Omega=\Omega_i\times\Omega_j\subset\mathbb{R}\times\mathbb{R}$ with $\mathbf{x}=(x_i,x_j)',$ $i,j\in I$ being the spatial coordinates. The dependent variable $d(t,\mathbf{x})=\begin{bmatrix} d_1(t,\mathbf{x}) & d_2(t,\mathbf{x}) & d_3(t,\mathbf{x}) \end{bmatrix}'$ is the input vector representing exogenous excitations or body forces, $\bar{\boldsymbol{u}}(t,\mathbf{x})=\begin{bmatrix} \bar{u}_1(t,\mathbf{x}) & \bar{u}_2(t,\mathbf{x}) & \bar{u}_3(t,\mathbf{x}) \end{bmatrix}'$ is the velocity vector, and $\bar{p}(t,\mathbf{x})$ is the pressure.

We consider perturbations (\boldsymbol{u},p) to the stationary flow (\boldsymbol{U},P) . That is,

$$\bar{\boldsymbol{u}} = \boldsymbol{u} + \boldsymbol{U}, \ \bar{p} = p + P,$$
 (2)

where (U, P) satisfy

$$0 = \frac{1}{Re} \nabla^2 \mathbf{U} - \mathbf{U} \cdot \nabla \mathbf{U} - \nabla P + F \mathbf{U},$$

$$0 = \nabla \cdot \mathbf{U}.$$
 (3)

Substituting (2) in (1) and using (3), we obtain the perturbation dynamics

$$\partial_{t} \boldsymbol{u} = \frac{1}{Re} \nabla^{2} \boldsymbol{u} - \boldsymbol{u} \cdot \nabla \boldsymbol{u} - \boldsymbol{U} \cdot \nabla \boldsymbol{u} - \boldsymbol{u} \cdot \nabla \boldsymbol{U} - \boldsymbol{v} \cdot \nabla \boldsymbol{u} - \boldsymbol{u} \cdot \nabla \boldsymbol{U} - \nabla \boldsymbol{v} + F \boldsymbol{u} + \boldsymbol{d},$$

$$0 = \nabla \cdot \boldsymbol{u}. \tag{4}$$

In this paper, we concentrate on perturbations with noslip boundary conditions $u|_{\partial\Omega}\equiv 0$ and periodic boundary conditions. B. Stability and Input-to-State Analysis

In this section, we briefly review a number of definitions and results from [17] and [18].

Definition 1 (Exponential Stability): The stationary solution $(0, p_0)$ of (4) with $d \equiv 0$ is exponentially stable in \mathcal{L}_{Ω}^2 , if there exists a $\lambda > 0$, such that for all $t \geq 0$

$$\|\boldsymbol{u}(t, \mathbf{x})\|_{\mathcal{L}_{\mathcal{O}}^{2}}^{2} \leq \|\boldsymbol{u}(0, \mathbf{x})\|_{\mathcal{L}_{\mathcal{O}}^{2}}^{2} e^{-\lambda t}.$$
 (5)

That is, system (1) converges to the laminar flow (\boldsymbol{U}, P) as in (3).

Definition 2 (input-to-State Properties):

A. Induced \mathcal{L}^2 -norm Boundedness: For some $\eta_i > 0, i = 1, 2, 3,$

$$\|\boldsymbol{u}(t,\mathbf{x})\|_{\mathcal{L}^{2}_{[0,\infty),\Omega}} \le \sum_{i=1}^{3} \eta_{i} \|d_{i}(t,\mathbf{x})\|_{\mathcal{L}^{2}_{[0,\infty),\Omega}}$$
 (6)

subject to zero initial conditions $u(0, x) \equiv 0, \ \forall x \in \Omega$.

B. *Input-to-State Stability*: For some scalar $\psi > 0$, functions $\beta, \tilde{\beta}, \chi \in \mathcal{K}_{\infty}$, and $\sigma \in \mathcal{K}$, it holds that

$$\|\boldsymbol{u}(t,\mathbf{x})\|_{\mathcal{L}_{\Omega}^{2}} \leq \beta \left(e^{-\psi t} \chi \left(\|\boldsymbol{u}(0,\mathbf{x})\|_{\mathcal{L}_{\Omega}^{2}}\right)\right) + \tilde{\beta} \left(\sup_{\tau \in [0,t)} \left(\iint_{\Omega} \sigma\left(|\boldsymbol{d}(\tau,\mathbf{x})|\right) d\Omega\right)\right), \quad (7)$$

for all t > 0.

Remark 1: Due to nonlinear dynamics, the actual induced \mathcal{L}^2 -norms of system (4) are nonlinear functions of $\|\boldsymbol{d}\|_{\mathcal{L}^2_\Omega}$. The quantities η_i , i=1,2,3 provide upper-bounds on the actual induced \mathcal{L}^2 -norms.

Remark 2: The ISS property (7) implies the exponential convergence to the laminar flow (U, P) in \mathcal{L}^2_{Ω} when $d \equiv 0$. Moreover, as $t \to \infty$, we obtain

$$\lim_{t \to \infty} \|\boldsymbol{u}(t, \mathbf{x})\|_{\mathcal{L}^{2}_{\Omega}} \leq \beta \left(\iint_{\Omega} \|\sigma(|\boldsymbol{d}(t, \mathbf{x})|)\|_{\mathcal{L}^{\infty}_{[0, \infty)}} d\Omega \right)
\leq \beta \left(\iint_{\Omega} \sigma(\|\boldsymbol{d}(t, \mathbf{x})\|_{\mathcal{L}^{\infty}_{[0, \infty)}}) d\Omega \right), \quad (8)$$

wherein, the fact that $\sigma, \beta \in \mathcal{K}$ is used. Hence, as long as the external excitations or body forces d are bounded in $\mathcal{L}^{\infty}_{[0,\infty)}$ (this encompasses persistent excitations), the perturbation velocities u are bounded in \mathcal{L}^{2}_{Ω} sense.

The next result converts the tests for exponential stability, induced \mathcal{L}^2 -norm boundedness, and ISS into the existence problem of a Lyapunov or a storage functional satisfying a set of inequalities.

Theorem 1: Consider perturbation model (4). If there exist a positive definite Lyapunov functional $V(\boldsymbol{u})$ and a positive semidefinite storage functional $S(\boldsymbol{u})$, positive scalars $\{\eta_i\}_{i\in\{1,2,3\}}, \{c_i\}_{i\in\{1,2,3\}}, \psi$, and functions $\beta_1,\beta_2\in\mathcal{K}_{\infty}$, $\sigma\in\mathcal{K}$, such that

I) when $d \equiv 0$,

$$c_1 \| \boldsymbol{u} \|_{\mathcal{L}^2_{\Omega}}^2 \le V(\boldsymbol{u}) \le c_2 \| \boldsymbol{u} \|_{\mathcal{L}^2_{\Omega}}^2,$$
 (9)

$$\partial_t V(\boldsymbol{u}) \le -c_3 \|\boldsymbol{u}\|_{\mathcal{L}_0^2}^2,\tag{10}$$

¹Invariance in one direction is a common assumption in the case of several fluid models, namely, Couette flow, Poiseuille flow, Taylor-Couette flow, etc.

II)

$$\partial_t S(\boldsymbol{u}) \le -\iint_{\Omega} \boldsymbol{u}' \boldsymbol{u} \, d\Omega + \iint_{\Omega} \boldsymbol{d}' \begin{bmatrix} \eta_1^2 & 0 & 0 \\ 0 & \eta_2^2 & 0 \\ 0 & 0 & \eta_3^2 \end{bmatrix} \boldsymbol{d} \, d\Omega, (11)$$

III)

$$\beta_1(\|\boldsymbol{u}\|_{\mathcal{L}^2_{\Omega}}) \le S(\boldsymbol{u}) \le \beta_2(\|\boldsymbol{u}\|_{\mathcal{L}^2_{\Omega}}),$$
 (12)

$$\partial_t S(\boldsymbol{u}) \le -\psi S(\boldsymbol{u}) + \iint_{\Omega} \sigma(|\boldsymbol{d}(t, \mathbf{x})|) \, d\Omega,$$
 (13)

for all t > 0, then, respectively, system (4)

I) is exponentially stable,

II) has induced \mathcal{L}^2 -norm upper-bounds η_i , i=1,2,3 as in (6),

III) is *ISS* and satisfies (7) with $\chi=\beta_2,\ \beta(\cdot)=\beta_1^{-1}\circ 2(\cdot)$ and $\tilde{\beta}(\cdot)=\beta_1^{-1}\circ\frac{2}{\psi}(\cdot)$.

Proof: This is a direct application of Theorem 1 in [17] and Theorem 1 in [18].

III. LYAPUNOV AND STORAGE FUNCTIONALS FOR FLUID FLOWS

In this section, we derive classes of Lyapunov and storage functionals suitable for analysis of system (4) subject to invariance in one of the three spatial coordinates. In the following, we adopt Einstein's multi-index notation over index j, that is the sum over repeated indices j, e.g., $v_j \partial_{x_j} u_j = \sum_j v_j \partial_{x_j} u_j$.

The perturbation model (4) can be re-written as

$$\partial_t u_i = \frac{1}{Re} \nabla^2 u_i - u_j \partial_{x_j} u_i - U_j \partial_{x_j} u_i - u_j \partial_{x_j} U_i - \partial_{x_i} p + F_{ij} u_j + d_i,$$

$$0 = \partial_{x_j} u_j. \tag{14}$$

where $i, j \in \{1, 2, 3\}$ and F_{ij} is the (i, j) entry of F.

The next theorem states, under which Lyapunov/storage functional structure, the time derivative of the Lyapunov/storage functional takes the form of a quadratic form in dependent variables \boldsymbol{u} and their spatial derivatives, by removing the nonlinear convection and pressure terms.

Proposition 1: Consider the perturbation model (14) subject to periodic or no-slip boundary conditions $u|_{\partial\Omega}=0$. Assume (14) is invariant with respect to $x_m, m \in \{1,2,3\}$. Let $I=\{1,2,3\}-\{m\}$ and

$$V(\boldsymbol{u}) = \frac{1}{2} \iint_{\Omega} \boldsymbol{u}' \begin{bmatrix} k_m & 0 & 0 \\ 0 & k_i & 0 \\ 0 & 0 & k_j \end{bmatrix} \boldsymbol{u} \, d\Omega$$
$$= \frac{1}{2} \iint_{\Omega} \sum_{i=1}^{3} k_i u_i(t, \mathbf{x})^2 \, d\Omega, \quad (15)$$

where $k_i = k_j$ for $i, j \in I$, be a candidate Lyapunov or storage functional. Then, the time derivative of (15) satisfies

$$\partial_t V(\boldsymbol{u}) \le -\sum_{i=1}^3 k_i \iint_{\Omega} \left(\frac{C(\Omega)}{Re} u_i^2 + U_j u_i \partial_{x_j} u_i + u_j u_i \partial_{x_j} U_i - u_i F_{ij} u_j \right) d\Omega, \quad (16)$$

where C > 0.

Proof: The time derivative of Lyapunov functional (15) along the solutions of (14) can be computed as

$$\partial_t V(\boldsymbol{u}) = \sum_{i=1}^3 \iint_{\Omega} k_i \left(\frac{1}{Re} u_i \nabla^2 u_i - u_j u_i \partial_{x_j} u_i - U_j u_i \partial_{x_j} u_i - u_j u_i \partial_{x_j} U_i - u_i \partial_{x_i} p + u_i F_{ij} u_j + u_i d_i \right) d\Omega.$$
(17)

Consider $\iint_{\Omega} k_i u_j u_i \partial_{x_j} u_i d\Omega$. Using the boundary conditions, integration by parts and the incompressibility condition $\partial_{x_j} u_j = 0$, we obtain

$$\iint_{\Omega} k_i u_j u_i \partial_{x_j} u_i \, d\Omega = \frac{1}{2} \int_{\Omega_i} k_i u_j u_i^2 |_{\partial \Omega_j} \, dx_i$$
$$-\frac{1}{2} \iint_{\Omega} k_i u_i^2 \left(\partial_{x_j} u_j \right) \, d\Omega = 0. \quad (18)$$

At this point, consider the pressure terms $\iint_{\Omega} k_i u_i \partial_{x_i} p \, d\Omega$. Without loss of generality, we consider invariance in x_1 , which yields

$$\iint_{\Omega} (k_2 u_2 \partial_{x_2} p + k_3 u_3 \partial_{x_3} p) \, d\Omega$$

$$= \int_{\Omega_3} (k_2 u_2 p)|_{\partial \Omega_2} \, dx_3 + \int_{\Omega_2} (k_3 u_3 p)|_{\partial \Omega_3} \, dx_2$$

$$- \iint_{\Omega} (k_2 \partial_{x_2} u_2 p + k_3 \partial_{x_3} u_3 p) \, d\Omega$$

$$= - \iint_{\Omega} (k_2 \partial_{x_2} u_2 + k_3 \partial_{x_3} u_3) p \, d\Omega, \quad (19)$$

where in the first equality above integration by parts and in the second inequality the boundary conditions are used. Then, if $k_2=k_3$, using the incompressibility condition $\partial_{x_2}u_2+\partial_{x_3}u_3=0$, (19) equals zero. Therefore, the time derivative of the Lyapunov/storage functional (17) is modified to

$$\partial_t V(\boldsymbol{u}) = \sum_{i=1}^3 \iint_{\Omega} k_i \left(\frac{1}{Re} u_i \nabla^2 u_i - U_j u_i \partial_{x_j} u_i - u_j u_i \partial_{x_j} U_i + u_i F_{ij} u_j + u_i d_i \right) d\Omega. \quad (20)$$

Integrating by parts the $u_i \nabla^2 u_i$ term and using the boundary conditions, we get

$$\partial_t V(\boldsymbol{u}) = \sum_{i=1}^3 \iint_{\Omega} k_i \left(\frac{1}{Re} (\partial_{x_i} u_i)^2 - U_j u_i \partial_{x_j} u_i - u_j u_i \partial_{x_j} U_i + u_i F_{ij} u_j + u_i d_i \right) d\Omega. \quad (21)$$

Applying Poincaré inequality (Lemma 1 in Appendix A) to (21), we obtain (16).

Remark 3: A special case of (15) was used in [19] to study the stability of viscous fluid flows.

Remark 4: In the sequel, we use structure (15) as a Lyapunov functional when studying stability and as a storage functional when studying input-to-state properties.

Remark 5: There are several estimates for the optimal Poincaré constant. The optimal constant we use in this paper is

$$C(\Omega) = \frac{\pi^2}{D(\Omega)},\tag{22}$$

where $D(\Omega)$ is the diameter of the domain Ω [20].

The next corollary proposes conditions under which properties such as stability, input-state induced \mathcal{L}^2 bounds and ISS can be inferred for the flow described by (14).

Corollary 1: Consider the flow described by (14) subject to periodic or no-slip boundary conditions $u|_{\partial\Omega}=0$. Assume the flow is invariant with respect to $x_m, m\in\{1,2,3\}$. Let $I=\{1,2,3\}-\{m\}$. If there exist positive constants $k_i, i=1,2,3$, with $k_i=k_j, i,j\in I$, positive scalars $\{\psi_i\}_{i\in\{1,2,3\}}, \{\eta\}_{i\in\{1,2,3\}}, \text{ and } \sigma\in\mathcal{K} \text{ such that } I)$ when $d\equiv 0$.

$$\sum_{i=1}^{3} k_i \iint_{\Omega} \left(\frac{C(\Omega)}{Re} u_i^2 + U_j u_i \partial_{x_j} u_i + u_j u_i \partial_{x_j} U_i - u_i F_{ij} u_j \right) d\Omega > 0$$
 (23)

II)

$$\sum_{i=1}^{3} \iint_{\Omega} \left(\left(\frac{k_i C(\Omega)}{Re} - 1 \right) u_i^2 + k_i U_j u_i \partial_{x_j} u_i + k_i u_j u_i \partial_{x_j} U_i - k_i u_i F_{ij} u_j - k_i u_i d_i + \eta_i^2 d_i^2 \right) d\Omega \ge 0$$
(24)

III)

$$\sum_{i=1}^{3} \iint_{\Omega} \left(\left(\frac{k_i C(\Omega)}{Re} - \psi_i k_i \right) u_i^2 + k_i U_j u_i \partial_{x_j} u_i + k_i u_j u_i \partial_{x_j} U_i - k_i u_i F_{ij} u_j - k_i u_i d_i + \sigma(|d_1|, |d_2|, |d_3|) \right) d\Omega \ge 0 \quad (25)$$

Then.

I) perturbation velocities given by (14) are exponentially stable. Therefore, the flow converges to the laminar flow exponentially.

II) under zero perturbation initial conditions $u(0, x) \equiv 0$, the induced \mathcal{L}^2 norm from inputs to perturbation velocities is bounded by η_i , $i \in \{1, 2, 3\}$ as in (6).

III) the perturbation velocities described by (14) are ISS in the sense of (7).

Proof: Each item is proven as follows.

I) Considering Lyapunov functional (15), inequality (9) is satisfied with $c_1 = \min_{i \in \{1,2,3\}} k_i$ and $c_2 = \max_{i \in \{1,2,3\}} k_i$. Re-arranging the terms in (23) gives

$$-\sum_{i=1}^{3} k_{i} \iint_{\Omega} \left(\frac{C(\Omega)}{Re} u_{i}^{2} + U_{j} u_{i} \partial_{x_{j}} u_{i} + u_{j} u_{i} \partial_{x_{j}} U_{i} - u_{i} F_{ij} u_{j} - u_{i} d_{i} \right) d\Omega < 0. \quad (26)$$

Then, from Proposition 1, we infer that, for $d \equiv 0$, $\partial_t V(\boldsymbol{u}) < 0$. By continuity, we infer that there exists $c_3 > 0$ such that (10) holds. Then, form Item I in Theorem 1, we infer that the perturbation velocities are exponentially stable. II) Re-arranging terms in (24) yields

$$-\sum_{i=1}^{3} k_{i} \iint_{\Omega} \left(\frac{C(\Omega)}{Re} u_{i}^{2} + U_{j} u_{i} \partial_{x_{j}} u_{i} + u_{j} u_{i} \partial_{x_{j}} U_{i} \right.$$
$$\left. - u_{i} F_{ij} u_{j} - u_{i} d_{i} \right) d\Omega$$
$$\leq -\sum_{i=1}^{3} \iint_{\Omega} u_{i}^{2} d\Omega + \sum_{i=1}^{3} \iint_{\Omega} \eta_{i}^{2} d_{i}^{2} d\Omega \quad (27)$$

Then, from (16) in Proposition 1, we deduce that

$$\partial_t V(\boldsymbol{u}) \le -\sum_{i=1}^3 \iint_{\Omega} u_i^2 d\Omega + \sum_{i=1}^3 \iint_{\Omega} \eta_i^2 d_i^2 d\Omega.$$

From Item II in Theorem 1, we infer that, under zero initial conditions, the perturbation velocities satisfy (6).

III) Adopting (15) as a storage functional, (12) is satisfied with $\beta_1(\cdot) = \min_{i \in \{1,2,3\}} k_i(\cdot)^2$ and $\beta_2(\cdot) = \max_{i \in \{1,2,3\}} k_i(\cdot)^2$. Re-arranging the terms in (25), we obtain

$$-\sum_{i=1}^{3} \iint_{\Omega} \left(\frac{k_{i}C(\Omega)}{Re} u_{i}^{2} + k_{i}U_{j}u_{i}\partial_{x_{j}}u_{i} + k_{i}u_{j}u_{i}\partial_{x_{j}}U_{i} - k_{i}u_{i}F_{ij}u_{j} - k_{i}u_{i}d_{i} \right) d\Omega$$

$$\leq -\sum_{i=1}^{3} \psi_{i} \iint_{\Omega} k_{i}u_{i}^{2} d\Omega + \iint_{\Omega} \sigma(|d_{1}|, |d_{2}|, |d_{3}|) d\Omega$$

$$(28)$$

From (16) in Proposition 1, it follows that

$$\partial_t V(\boldsymbol{u}) \leq -\psi V(\boldsymbol{u}) + \iint_{\Omega} \sigma(|d_1|, |d_2|, |d_3|) d\Omega, \quad (29)$$

with $\psi = \min_{i \in \{1,2,3\}} \psi_i$. Then, from Item III in Theorem 1, we infer that the perturbation velocities satisfy the ISS property (7).

IV. CONVEX FORMULATION FOR STREAMWISE CONSTANT FLOWS

To present a convex method for checking the conditions in Corollary 1, we restrict our attention to streamwise constant flows in x_m -direction with laminar flow $U = U_m(x) \overrightarrow{e}_m$.

Corollary 2: Consider the perturbation dynamics given by (14). Assume streamwise invariance in x_m -direction with laminar flow $U = U_m(\mathbf{x}) \overrightarrow{e}_m$ where $m \in \{1,2,3\}$. Let $I = \{1,2,3\} - \{m\}$. If there exist positive constants $\{k_l\}_{l \in \{1,2,3\}}$ with $k_p = k_q$, $p,q \in I$, $\{\eta_l\}_{l \in \{1,2,3\}}$, $\{\psi_l\}_{l \in \{1,2,3\}}$, and functions $\{\sigma_l\}_{l \in \{1,2,3\}}$ such that I) (30) holds,

$$M(\mathbf{x}) = \begin{bmatrix} \left(\frac{C}{Re} - F_{mm}\right) k_m & \frac{k_m(\partial_{x_j} U_m(\mathbf{x}) - F_{mj}) - k_j F_{jm}}{2} & \frac{k_m(\partial_{x_i} U_m(\mathbf{x}) - F_{mi}) - k_i F_{im}}{2} \\ \frac{k_m(\partial_{x_j} U_m(\mathbf{x}) - F_{mi}) - k_i F_{im}}{2} & \left(\frac{C}{Re} - F_{jj}\right) k_j & -\frac{k_j F_{jm}}{2} \\ -\frac{k_j F_{jm}}{2} & \left(\frac{C}{Re} - F_{ii}\right) k_i \end{bmatrix} \ge 0, \ i, j \in I, i \ne j, \ \mathbf{x} \in \Omega.$$
(30)

II)

$$N(\mathbf{x}) = \begin{bmatrix} & & -\frac{k_m}{2} & 0 & 0\\ M(\mathbf{x}) - \mathbf{I}_{3\times3} & & 0 & -\frac{k_j}{2} & 0\\ & & 0 & 0 & -\frac{k_i}{2} & 0\\ -\frac{k_m}{2} & 0 & 0 & \eta_m^2 & 0 & 0\\ 0 & -\frac{k_j}{2} & 0 & 0 & \eta_i^2 & 0\\ 0 & 0 & -\frac{k_i}{2} & 0 & 0 & \eta_j^2 \end{bmatrix} \ge 0, \quad (31)$$

for $i, j \in I, i \neq j$ and $\mathbf{x} \in \Omega$, III) $\sigma_l(\mathbf{x}) \geq 0, \ \mathbf{x} \in \Omega, \ l \in \{1, 2, 3\}$ and

$$P(\mathbf{x}) = \begin{bmatrix} & & -\frac{k_m}{2} & 0 & 0\\ & M(\mathbf{x}) - Q & 0 & -\frac{k_j}{2} & 0\\ & & 0 & 0 & -\frac{k_j}{2} & 0\\ -\frac{k_m}{2} & 0 & 0 & \sigma_m(\mathbf{x}) & 0 & 0\\ 0 & -\frac{k_j}{2} & 0 & 0 & \sigma_j(\mathbf{x}) & 0\\ 0 & 0 & -\frac{k_i}{2} & 0 & 0 & \sigma_i(\mathbf{x}) \end{bmatrix} \ge 0,$$

$$(32)$$

 $\text{for } i,j \in I, i \neq j \text{ and } \mathbf{x} \in \Omega, \text{ where } Q = \begin{bmatrix} \psi_m k_m & 0 & 0 \\ 0 & \psi_j k_j & 0 \\ 0 & 0 & \psi_i k_i \end{bmatrix}.$ Then, it follows that

Then, it follows that

- I) the perturbation velocities are exponentially stable,
- II) subject to zero initial conditions, the induced \mathcal{L}^2 norm from inputs to perturbation velocities is bounded by η_i , i = 1, 2, 3 as in (6),
- III) the perturbation velocities are ISS in the sense of (7) with $\sigma(|\mathbf{d}|) = \sum_{i=1}^3 \sigma_i(\mathbf{x}) d_i^2$.

Proof: The proof is straightforward and follows from computing conditions (23), (27), and (25) considering x_m -invariance, the laminar flow $\boldsymbol{U} = U_m \overrightarrow{e}_m$, and $\sigma(|\boldsymbol{d}|) = \sum_{i=1}^3 \sigma_i(\mathbf{x}) d_i^2$. Since the flow is x_m -invariant and the laminar flow is given by $\boldsymbol{U} = U_m \overrightarrow{e}_m$, $U_j u_i \partial_{x_j} u_i = 0$, i = 1, 2, 3.

I) Inequality (23) is given by

$$\mathcal{A} = \iint_{\Omega} \left(\left(\frac{C(\Omega)}{Re} - F_{ii} \right) k_i u_i^2 - u_i (k_i F_{ij}) u_j - u_i (k_i F_{im}) u_m \right.$$

$$\left. + \left(\frac{C(\Omega)}{Re} - F_{jj} \right) k_j u_j^2 - u_j (k_j F_{ji}) u_i - u_j (k_j F_{jm}) u_m \right.$$

$$\left. \left(\frac{C(\Omega)}{Re} - F_{mm} \right) k_m u_m^2 + u_m (\partial_{x_i} U_m - F_{mi}) u_i \right.$$

$$\left. + u_m (\partial_{x_j} U_m - F_{mj}) \right) d\Omega \ge 0 \quad (33)$$

for $i, j \in I$, $i \neq j$, which can be rewritten as

$$\iint_{\Omega} \begin{bmatrix} u_m \\ u_j \\ u_i \end{bmatrix}' M(\mathbf{x}) \begin{bmatrix} u_m \\ u_j \\ u_i \end{bmatrix} d\Omega \ge 0.$$
 (34)

with M(x) given in (30). Therefore, if (30) is satisfied, (34) also holds and from Item I in Corollary 1 we infer that the perturbation velocities are exponentially stable.

II) Inequality (27) is changed to

$$\mathcal{A} + \iint_{\Omega} (k_i u_i d_i + k_j u_j d_j + k_m u_m d_m) \, d\Omega$$
$$- \iint_{\Omega} (u_i^2 + u_j^2 + u_m^2) \, d\Omega$$
$$+ \iint_{\Omega} (\eta_i^2 d_i^2 + \eta_j^2 d_j^2 + \eta_m^2 d_m^2) \, d\Omega \ge 0, \quad (35)$$

for $i, j \in I$, $i \neq j$, which can be rewritten as

$$\iint_{\Omega} \begin{bmatrix} u_m \\ u_j \\ u_i \\ d_m \\ d_j \\ d_d \end{bmatrix}' N(\mathbf{x}) \begin{bmatrix} u_m \\ u_j \\ u_i \\ d_m \\ d_j \\ d_d \end{bmatrix} d\Omega \ge 0, \tag{36}$$

where N is defined in (31). Consequently, if (31) is satisfied for all $x \in \Omega$, (36) holds and from Item II in Corollary 1 we infer that, subject to zero initial conditions, the induced \mathcal{L}^2 norm from inputs to perturbation velocities is bounded by η_i , i=1,2,3 as in (6).

III) The proof follows the same lines as the proof of Item II above.

In the case that $U_m(\mathbf{x})$ is a polynomial in \mathbf{x} , inequalities (30), (31), and (32) are polynomial matrix inequalities that should be checked for all $\mathbf{x} \in \Omega$. If the set Ω is a semi-algebraic set then these inequalities can be cast as a sum-of-squares (SOS) program (see Appendix B) by using Putinar's Positivstellensatz theorem [21, Theorem 2.14].

Remark 6: In order to find upper-bounds on the induced \mathcal{L}^2 -norm from the body forces (d_1, d_2, d_3) to the perturbation

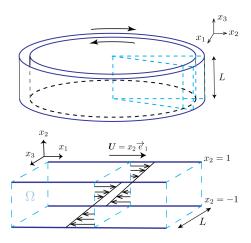


Fig. 1: Schematic of the rotating Couette flow geometry.

velocities u, we solve the following optimization problem

$$\min_{k_i,k_i} (\eta_1^2 + \eta_2^2 + \eta_3^2)$$

subject to $N(x) \ge 0, \ k_i, k_j > 0, \ i, j \in I.$ (37)

In the next section, we consider the analysis of the rotating Couette flow, which illustrate the proposed results.

V. EXAMPLE: ROTATING COUETTE FLOW

We consider the flow of viscous fluid between two co-axial cylinders, where the gap between the cylinders is much smaller than their radii. In this setting, the flow can be schematically illustrated as in Figure 1. The axis of rotation is parallel to x_3 -axis and the circumferential direction corresponds to x_1 -axis. Then, the dynamics of the perturbation velocities is described by (4). The flow is assumed to be invariant with respect to x_1 ($\partial_{x_1} = 0$) and periodic in x_3 with period L. Therefore, $\Omega = \{(x_2, x_3) \mid (x_2, x_3) \in [-1, 1] \times [0, L]\}$. The laminar flow is given by $U = (x_2, 0, 0)' = x_2 \overrightarrow{e}_1$ and $P = P_0$. In addition,

$$F = \begin{bmatrix} 0 & Ro & 0 \\ -Ro & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix},$$

where $Ro \in [0,1]$ is a parameter representing the Coriolis force². We consider no-slip boundary conditions $\boldsymbol{u}|_{x_2=-1}^1=0$ and $\boldsymbol{u}(t,x_2,x_3)=\boldsymbol{u}(t,x_2,x_3+L)$. The Poincaré constant is then given by $C=\frac{\pi^2}{L^2+2^2}$.

Notice that the cases Ro=0,1 correspond to the Couette flow. Thus, the obtained results for rotating Couette flow can be applied to the Couette flow in special cases, as well. We are interested in finding estimates of the critical Reynolds number Re_C using the following Lyapunov functional

$$V(u) = \int_0^L \int_{-1}^1 \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix}' \begin{bmatrix} k_1 & 0 & 0 \\ 0 & k_2 & 0 \\ 0 & 0 & k_2 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix} dx_2 dx_3,$$

which is the same as Lyapunov functional (15) considering invariance with respect to x_1 .

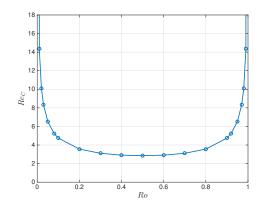


Fig. 2: Estimated critical Reynolds numbers Re in terms of Ro for rotating Couette flow.

For stability analysis, we need to check inequality (30) according to Item I in Corollary 2. For this flow (m = 1, j = 2, i = 3), we have

$$M = \begin{bmatrix} \frac{k_1 C}{Re} & \frac{k_2 Ro - k_1 (Ro - 1)}{2} & 0\\ \frac{k_2 Ro - k_1 (Ro - 1)}{2} & \frac{k_2 C}{Re} & 0\\ 0 & 0 & \frac{k_2 C}{Re} \end{bmatrix} \ge 0 \quad (38)$$

This is a linear matrix inequality (LMI) feasibility problem with decision variables $k_1, k_2 > 0$.

To find estimates of Re_C in the case of Couette Flow Ro=0, applying Schur complement theorem [22, p. 650] to (38), we have

$$\frac{k_1C}{Re} - \left(\frac{k_1}{2}\right)^2 \left(\frac{Re}{k_2C}\right) \ge 0, \ \frac{k_2C}{Re} \ge 0,$$

which yields the inequality

$$\frac{k_2}{k_1} \ge \left(\frac{Re}{2C}\right)^2. \tag{39}$$

This implies that the Couette flow is stable for all Re. Hence, for Couette flow, $Re_C = \infty$ obtained using Lyapunov functional (15) coincides with linear stability limit $Re_L = \infty$ [4].

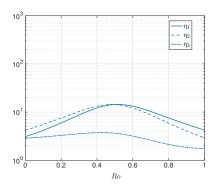
Let $L=\pi$. Figure 2 illustrates the estimated critical Reynolds numbers Re_C as a function of Ro obtained from solving the LMI (38) and performing a line search over Re. Notice that for the cases Ro=0,1 the flow is stable for all Reynolds numbers.

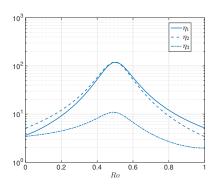
For induced \mathcal{L}^2 -norm analysis, we apply inequality (31) which for this particular flow is given by the following LMI

$$N = \begin{bmatrix} & & -\frac{k_1}{2} & 0 & 0\\ M - I_{3\times 3} & & 0 & -\frac{k_2}{2} & 0\\ & & & 0 & 0 & -\frac{k_2}{2} & 0\\ -\frac{k_1}{2} & 0 & 0 & \eta_1^2 & 0 & 0\\ 0 & -\frac{k_2}{2} & 0 & 0 & \eta_2^2 & 0\\ 0 & 0 & -\frac{k_2}{2} & 0 & 0 & \eta_3^2 \end{bmatrix} \ge 0$$

 $^{^2}$ That is, Ro=0 (Ro=1) corresponds to the case where only the outer (inner) cylinder is rotating and Ro=0.5 is the case where both cylinders are rotating with the same velocity but in opposite direction.

 $^{^3}$ For Ro=1, we can similarly obtain $\frac{k_1}{k_2} \geq \left(\frac{Re}{2C}\right)^2$.





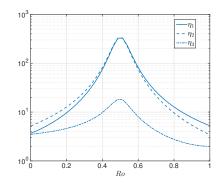


Fig. 3: Upper bounds on induced \mathcal{L}^2 -norms from \boldsymbol{d} to perturbation velocities \boldsymbol{u} of rotating Couette flow for different Reynolds numbers: Re=2 (left), Re=2.8 (middle), and Re=2.83 (right).

with M as in (38).

Figure 3 depicts the obtained results for three different Reynolds numbers. As the Reynolds number approaches the estimated Re_C for Ro=0.5, the upper-bounds on the induced \mathcal{L}^2 -norm from the body forces d to perturbation velocities u increases dramatically.

The obtained upper-bounds on the induced \mathcal{L}^2 -norm for Couette flow Ro=0, are also given in Figure 4. Since the flow is stable for all Reynolds numbers, the induced \mathcal{L}^2 -norms keep increasing with Reynolds number. The obtained upper-bounds depicted in Figure 4 are consistent with Corollary 2 and Corollary 4 in [13] and Theorem 1 in [12], wherein it was demonstrated that $\eta_1^2 \propto O(Re)$, and $\eta_2^2, \eta_3^2 \propto O(Re^3)$ for Couette flow.

In order to check the ISS property, we check inequality (32) from Corollary 2 for the rotating Couette flow under study, i.e.,

$$P = \begin{bmatrix} & & -\frac{k_1}{2} & 0 & 0\\ M - Q & 0 & -\frac{k_2}{2} & 0\\ & & 0 & 0 & -\frac{k_2}{2} \\ -\frac{k_1}{2} & 0 & 0 & \sigma_1 & 0 & 0\\ 0 & -\frac{k_2}{2} & 0 & 0 & \sigma_2 & 0\\ 0 & 0 & -\frac{k_2}{2} & 0 & 0 & \sigma_3 \end{bmatrix} \ge 0$$

with M given in (38) and $Q=\begin{bmatrix}k_1\psi_1&0&0\\0&k_2\psi_2&0\\0&0&k_2\psi_3\end{bmatrix}$. We fix $\psi_i=10^{-4},\ i=1,2,3$ and $L=2\pi.$ Figure 5 depicts the maximum Reynolds number for which ISS certificates could be found Re_{ISS} and stability critical Reynold's numbers Re_C as a function of Ro. It appears that for $Ro\in(0,1)$ these two quantities coincide. However, for the case of Couette flow Ro=0,1, we obtain $Re_{ISS}=316$ and $Re_C=\infty.$ The quantity $Re_{ISS}=316$ is the closest estimate to the empirical Reynolds number $Re\approx350$ [5].

VI. CONCLUSIONS AND FUTURE WORK

A. Conclusions

We studied stability and input-state properties of fluid flows with invariance in one direction. We formulated a

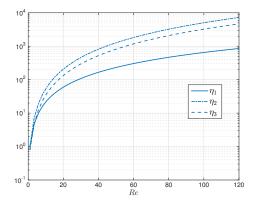


Fig. 4: Upper bounds on induced \mathcal{L}^2 -norms for perturbation velocities of Couette flow for different Reynolds numbers.

class of appropriate Lyapunov/storage functionals for such flows. Conditions based on matrix inequalities are given for streamwise constant flows. When the laminar flow is given by a polynomial of spatial coordinates, the matrix inequalities can be checked using convex optimization. For illustration purposes, we applied the proposed method to study a model of rotating Couette flow.

B. Future Work

In this study, we considered flows in the Cartesian coordinate system. For many flows, like pipe Poiseuille flow, the coordinate system is naturally cylindrical. An extension of the results proposed in this paper to cylindrical coordinates is under study.

In several scenarios in fluid mechanics, we are interested in a functional of the perturbation dynamics. For example, in the drag estimation problem, we are interested in estimating the functional of pressure over the surface of an airfoil. We are currently applying the methodology proposed in [23] to address such problems in fluid mechanics.

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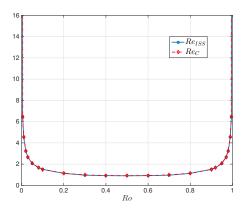


Fig. 5: Estimated critical Reynolds numbers Re_C and ISS Reynolds numbers Re_{ISS} in terms of Ro.

perial College London and Prof. Charles Doering, from Department of Mathematics, University of Michigan.

REFERENCES

- P. G. Drazin and W. H. Reid, Hydrodynamic Stability. New York Cambridge University Press, 1981.
- [2] D. D. Joseph, Stability of fluid motions, ser. Springer Tracts in Natural Philosophy. Berlin: Springer-Verlag, 1976.
- [3] J. Serrin, "On the stability of viscous fluid motions," Arch. Ration. Mech. Anal., vol. 3, pp. 1–13, 1959.
- [4] V. Romanov, "Stability of plane-parallel Couette flow," Functional Analysis and Its Applications, vol. 7, no. 2, pp. 137–146, 1973.
- [5] N. Tillmark and P. H. Alfredsson, "Experiments on transition in plane Couette flow," *Journal of Fluid Mechanics*, vol. 235, pp. 89–102, 1992.
- [6] L. N. Trefethen, A. E. Trefethen, S. C. Reddy, and T. A. Driscoll, "Hydrodynamic stability without eigenvalues," *Science*, vol. 261, no. 5121, pp. 578–584, 1993.
- [7] P. J. Schmid, "Nonmodal stability theory," Annual Review of Fluid Mechanics, vol. 39, no. 1, pp. 129–162, 2007.
- [8] P. J. Goulart and S. Chernyshenko, "Global stability analysis of fluid flows using sum-of-squares," *Physica D: Nonlinear Phenomena*, vol. 241, no. 6, pp. 692 – 704, 2012.
- [9] S. Chernyshenko, P. Goulart, D. Huang, and A. Papachristodoulou, "Polynomial sum of squares in fluid dynamics: a review with a look ahead," *Royal Society of London. Philosophical Transactions A. Mathematical, Physical and Engineering Sciences*, vol. 372, no. 2020, 2014.
- [10] O. Reynolds, "An experimental investigation of the circumstances which determine whether the motion of water shall be direct or sinuous and the law of resistance in parallel channels," *Philos. Trans.*, vol. 935, no. 51, 1883.
- [11] B. F. Farrell and P. J. Ioannou, "Stochastic forcing of the linearized Navier-Stokes equations," *Physics of Fluids A*, vol. 5, no. 11, pp. 2600– 2609, 1993.
- [12] B. Bamieh and M. Dahleh, "Energy amplification in channel flows with stochastic excitation," *Physics of Fluids*, vol. 13, no. 11, pp. 3258–3269, 2001.
- [13] M. R. Jovanović and B. Bamieh, "Componentwise energy amplification in channel flows," *Journal of Fluid Mechanics*, vol. 534, pp. 145–183, 2005.
- [14] M. R. Jovanović, "Modeling, analysis, and control of spatially distributed systems," Ph.D. dissertation, University of California, Santa Barbara. 2004.
- [15] D. F. Gayme, B. J. McKeon, B. Bamieh, A. Papachristodoulou, and J. C. Doyle, "Amplification and nonlinear mechanisms in plane Couette flow," *Physics of Fluids*, vol. 23, no. 6, 2011.
- [16] M. Jovanović and B. Bamieh, "The spatio-temporal impulse response of the linearized Navier-Stokes equations," in *Proceedings of 2001 American Control Conference*, vol. 3, June 2001, pp. 1948–1953.

- [17] G. Valmorbida, M. Ahmadi, and A. Papachristodoulou, "Semi-definite programming and functional inequalities for distributed parameter systems," in 53rd Conference on Decision and Control, Los Angeles, CA, 2014.
- [18] M. Ahmadi, G. Valmorbida, and A. Papachristodoulou, "Input-output analysis of distributed parameter systems using convex optimization," in *Decision and Control (CDC)*, 2014 IEEE 53rd Annual Conference on, Dec 2014, pp. 4310–4315.
- [19] D. D. Joseph and W. Hung, "Contributions to the nonlinear theory of stability of viscous flow in pipes and between rotating cylinders," *Archive for Rational Mechanics and Analysis*, vol. 44, no. 1, pp. 1–22, 1971.
- [20] L. Payne and H. Weinberger, "An optimal poincare inequality for convex domains," *Archive for Rational Mechanics and Analysis*, vol. 5, no. 1, pp. 286–292, 1960.
- [21] J. B. Lasserre, Moments, Positive Polynomials and Their Applications. Imperial College Press, London, 2009.
- [22] S. Boyd and L. Vandenberghe, Convex Optimization. Cambridge University Press, 2004.
- [23] M. Ahmadi, G. Valmorbida, and A. Papachristodoulou, "Barrier functionals for output functional estimation of PDEs," in 2015 American Control Conference, July 2015.
- [24] P. Parrilo, "Structured semidefinite programs and semialgebraic geometry methods in robustness and optimization," Ph.D. dissertation, California Institute of Technology, 2000.
- [25] M. Choi, T. Lam, and B. Reznick, "Sums of squares of real polynomials," in *Symposia in Pure Mathematics*, vol. 58, no. 2, 1995, pp. 103–126.
- [26] G. Chesi, A. Tesi, A. Vicino, and R. Genesio, "On convexification of some minimum distance problems," in 5th European Control Conference, Karlsruhe, Germany, 1999.
- [27] A. Papachristodoulou, J. Anderson, G. Valmorbida, S. Prajna, P. Seiler, and P. A. Parrilo, SOSTOOLS: Sum of squares optimization toolbox for MATLAB, http://arxiv.org/abs/1310.4716, 2013, available from http://www.eng.ox.ac.uk/control/sostools.

APPENDIX

A. Poincaré Inequality

Lemma 1 ([20]): Assume $\Omega \subset \mathbb{R}^2$ is a bounded, convex, Lipschitz domain with diameter D, and $u \in \mathcal{C}^1(\Omega)$ with noslip $u|_{\partial\Omega}=0$ or periodic such that $\iint_\Omega u \ d\Omega=0$ boundary conditions. Then, the following inequality holds

$$\frac{\pi}{D} \|u\|_{\mathcal{L}^2_{\Omega}} \le \|\nabla u\|_{\mathcal{L}^2_{\Omega}}.$$

B. Sum-of-Squares Programming

Denote the ring of polynomials with real coefficients by $\mathcal{R}[x]$, and the ring of polynomials with a sum-of-squares decomposition by $\Sigma[x] \subset \mathcal{R}[x]$. A polynomial $p(x) \in \Sigma[x]$ if $\exists p_i(x) \in \mathcal{R}[x], i \in \{1,\ldots,n_d\}$ such that $p(x) = \sum_{i=1}^{n_d} p_i^2(x)$. Hence, p(x) is clearly non-negative. The set of polynomials $\{p_i\}_{i=1}^{n_d}$ is called *SOS decomposition* of p(x). The converse does not hold in general, that is, there exist nonnegative polynomials which do not have an SOS decomposition [24]. To test whether an SOS decomposition exists for a given polynomial, one can solve an SDP (see [25], [24], [26]). SOSTOOLS [27] is a software package for solving SOS programs.